

Acta Crystallographica Section E

## Structure Reports

Online

ISSN 1600-5368

6*H*,12*H*-5,11-Ethano-dibenzo[*b,f*][1,5]-diazocineMasoud Faroughi,<sup>a</sup> Andrew C. Try<sup>a\*</sup> and Peter Turner<sup>b</sup><sup>a</sup>Department of Chemistry and Biomolecular Sciences, Building F7B, Macquarie University, NSW 2109, Australia, and <sup>b</sup>Crystal Structure Analysis Facility, School of Chemistry, F11, University of Sydney, NSW 2006, Australia

Correspondence e-mail: andrew.try@mq.edu.au

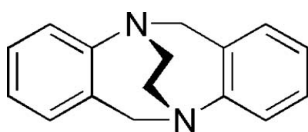
Received 7 January 2008; accepted 10 January 2008

Key indicators: single-crystal X-ray study; *T* = 150 K; mean  $\sigma(\text{C}-\text{C})$  = 0.002 Å; *R* factor = 0.038; *wR* factor = 0.100; data-to-parameter ratio = 17.9.

In the molecule of the title compound, C<sub>16</sub>H<sub>16</sub>N<sub>2</sub>, the ethano-strapped analogue of unsubstituted Tröger's base, the dihedral angle between the two benzene rings is 75.85 (4)°, the smallest angle measured for an ethano-strapped analogue.

## Related literature

For related literature, see: Hamada & Mukai (1996); Ishida *et al.* (2005); Solano *et al.* (2005); Faroughi *et al.* (2006*a,b*); Faroughi, Try & Turner (2007); Faroughi, Jensen & Try (2007). For related structures, see: Faroughi, Try, Klepetko *et al.* (2007); Faroughi *et al.* (2008).



## Experimental

## Crystal data

C<sub>16</sub>H<sub>16</sub>N<sub>2</sub>*M<sub>r</sub>* = 236.31Orthorhombic, *Pbca**a* = 11.717 (2) Å*b* = 8.907 (2) Å*c* = 22.829 (4) Å*V* = 2382.5 (8) Å<sup>3</sup>*Z* = 8Mo *K*α radiation $\mu$  = 0.08 mm<sup>-1</sup>*T* = 150 (2) K

0.43 × 0.42 × 0.15 mm

## Data collection

Bruker SMART 1000 CCD

diffractometer

Absorption correction: Gaussian

(Coppens *et al.*, 1965) and*XPREP* (Siemens, 1995)*T*<sub>min</sub> = 0.968, *T*<sub>max</sub> = 0.990

21723 measured reflections

2913 independent reflections

2398 reflections with *I* > 2σ(*I*)*R*<sub>int</sub> = 0.039

## Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.037$  $wR(F^2) = 0.099$ *S* = 1.03

2913 reflections

163 parameters

H-atom parameters constrained

 $\Delta\rho_{\text{max}} = 0.29 \text{ e } \text{Å}^{-3}$  $\Delta\rho_{\text{min}} = -0.20 \text{ e } \text{Å}^{-3}$ 

Data collection: *SMART* (Siemens, 1995); cell refinement: *SAINT* (Siemens, 1995); data reduction: *SAINT* and *XPREP* (Siemens, 1995); program(s) used to solve structure: *SIR97* (Altomare *et al.*, 1999); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *TEXSAN* (Molecular Structure Corporation, 1998), *Xtal3.6* (Hall *et al.*, 1999), *ORTEPII* (Johnson, 1976) and *WinGX* (Farrugia, 1999); software used to prepare material for publication: *WinGX*.

The authors thank the Australian Research Council for a Discovery Project grant to ACT (grant No. DP0345180) and Macquarie University for the award of a Macquarie University Research Development grant.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: TK2243).

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## supporting information

*Acta Cryst.* (2008). E64, o458 [doi:10.1107/S1600536808000883]

**6H,12H-5,11-Ethanodibenzo[*b,f*][1,5]diazocine**

Masoud Faroughi, Andrew C. Try and Peter Turner

**S1. Comment**

Tröger's base compounds related to the title compound, (I), Fig. 1, are formed from an acid catalysed condensation of anilines, or a range of other amino aromatics, with either formaldehyde or formaldehyde equivalents. The compounds are characterized by the presence of a methano-strapped diazocine ring that is fused to two aromatic rings and this strapped ring system imparts a V-shaped structure on the compounds. The dihedral angle between the aromatic rings has been measured for over 20 simple dibenzo Tröger's base analogues and has been found to lie between 82° (Solano *et al.*, 2005) and 108° (Faroughi *et al.*, 2006*b*). It has been shown that reaction of 1,2-dibromoethane with several Tröger's base compounds affords ethano-strapped analogues (Hamada & Mukai, 1996; Ishida *et al.*, 2005; Faroughi *et al.*, 2007*a*; Faroughi *et al.*, 2008), as outlined in Fig. 2. The structure of (I) is the third reported structure of an ethano-strapped analogue of Tröger's base. All three structures support the results of molecular modelling studies, which predict that the ethano-strapped analogues should have smaller dihedral angles in comparison with their methano-strapped precursors. The size of the angle for the methano-strapped structures (2,8-dibromo, 2,8-dichloro and unsubstituted, respectively) are as follows: 95° (Faroughi *et al.*, 2006*a*), 96° (Faroughi *et al.*, 2007*b*) and 95° (Faroughi, Jensen & Try, 2007), whilst the corresponding values for the ethano-strapped structures are 86° (Faroughi *et al.*, 2007*a*), 87° (Faroughi *et al.*, 2008) and, for the subject of this report, (I) 76°.

**S2. Experimental**

The title compound was prepared according to the literature procedure (Hamada & Mukai, 1996) in 37% yield. Single crystals were produced from slow evaporation of a dichloromethane solution of (I).

**S3. Refinement**

H atoms were positioned geometrically, with C—H = 0.95 and 0.99 Å for aromatic and methylene H atoms, respectively, and constrained to ride on their parent atoms, with  $U_{\text{iso}}(\text{H}) = 1.2U_{\text{eq}}(\text{C})$ .

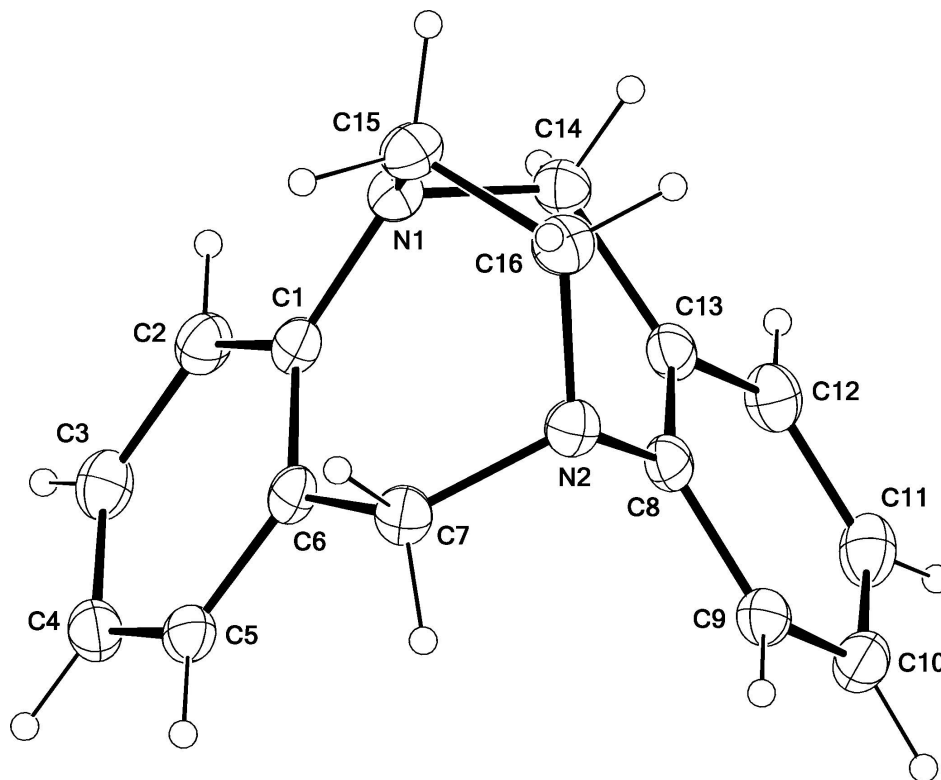


Figure 1

View of (I), showing the atomic numbering scheme. Displacement ellipsoids are shown at the 50% probability level.

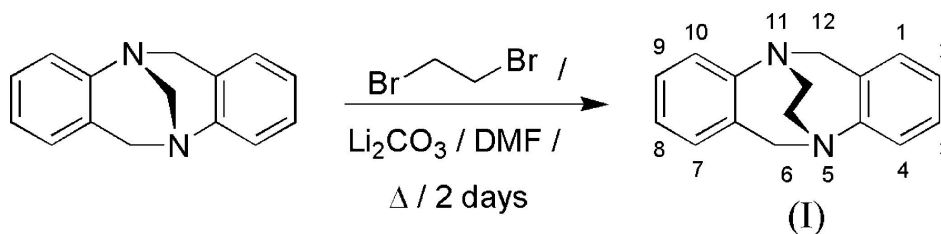


Figure 2

Synthetic scheme for the synthesis of (I) showing the numbering system used in naming the compound.

### 6*H*,12*H*-5,11-Ethanodibenzo[*b,f*][1,5]diazocine

#### Crystal data

$C_{16}H_{16}N_2$

$M_r = 236.31$

Orthorhombic, *Pbca*

Hall symbol: -P 2ac 2ab

$a = 11.717$  (2) Å

$b = 8.907$  (2) Å

$c = 22.829$  (4) Å

$V = 2382.5$  (8) Å<sup>3</sup>

$Z = 8$

$F(000) = 1008$

$D_x = 1.318$  Mg m<sup>-3</sup>

Melting point: 447 K

Mo  $K\alpha$  radiation,  $\lambda = 0.71073$  Å

Cell parameters from 985 reflections

$\theta = 2.5$ – $27.9^\circ$

$\mu = 0.08$  mm<sup>-1</sup>

$T = 150$  K

Plate, colourless

$0.43 \times 0.42 \times 0.15$  mm

Data collection

Bruker SMART 1000 CCD  
 diffractometer  
 Radiation source: fine-focus sealed tube  
 Graphite monochromator  
 $\omega$  scans  
 Absorption correction: gaussian  
 (Coppens *et al.*, 1965) and XPREP (Siemens,  
 1995)  
 $T_{\min} = 0.968$ ,  $T_{\max} = 0.990$

21723 measured reflections  
 2913 independent reflections  
 2398 reflections with  $I > 2\sigma(I)$   
 $R_{\text{int}} = 0.039$   
 $\theta_{\max} = 28.3^\circ$ ,  $\theta_{\min} = 1.8^\circ$   
 $h = -15 \rightarrow 15$   
 $k = -11 \rightarrow 11$   
 $l = -29 \rightarrow 28$

Refinement

Refinement on  $F^2$   
 Least-squares matrix: full  
 $R[F^2 > 2\sigma(F^2)] = 0.037$   
 $wR(F^2) = 0.099$   
 $S = 1.03$   
 2913 reflections  
 163 parameters  
 0 restraints  
 Primary atom site location: structure-invariant  
 direct methods

Secondary atom site location: difference Fourier  
 map  
 Hydrogen site location: inferred from  
 neighbouring sites  
 H-atom parameters constrained  
 $w = 1/[\sigma^2(F_o^2) + (0.0474P)^2 + 0.8505P]$   
 where  $P = (F_o^2 + 2F_c^2)/3$   
 $(\Delta/\sigma)_{\max} < 0.001$   
 $\Delta\rho_{\max} = 0.29 \text{ e } \text{Å}^{-3}$   
 $\Delta\rho_{\min} = -0.20 \text{ e } \text{Å}^{-3}$

Special details

**Geometry.** All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement.** Refinement of  $F^2$  against ALL reflections. The weighted  $R$ -factor  $wR$  and goodness of fit  $S$  are based on  $F^2$ , conventional  $R$ -factors  $R$  are based on  $F$ , with  $F$  set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating  $R$ -factors(gt) *etc.* and is not relevant to the choice of reflections for refinement.  $R$ -factors based on  $F^2$  are statistically about twice as large as those based on  $F$ , and  $R$ -factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters ( $\text{Å}^2$ )

|     | <i>x</i>      | <i>y</i>      | <i>z</i>    | $U_{\text{iso}}^*/U_{\text{eq}}$ |
|-----|---------------|---------------|-------------|----------------------------------|
| N1  | 0.12902 (7)   | 0.27164 (10)  | 0.17143 (4) | 0.0194 (2)                       |
| N2  | 0.04073 (7)   | -0.01939 (10) | 0.19142 (4) | 0.0194 (2)                       |
| C1  | 0.01598 (9)   | 0.29851 (11)  | 0.15021 (5) | 0.0187 (2)                       |
| C2  | 0.00104 (9)   | 0.42146 (12)  | 0.11285 (5) | 0.0222 (2)                       |
| H2  | 0.0648        | 0.4824        | 0.1031      | 0.027*                           |
| C3  | -0.10531 (10) | 0.45585 (12)  | 0.08975 (5) | 0.0244 (2)                       |
| H3  | -0.1138       | 0.5389        | 0.0640      | 0.029*                           |
| C4  | -0.19937 (9)  | 0.36838 (12)  | 0.10442 (5) | 0.0229 (2)                       |
| H4  | -0.2729       | 0.3929        | 0.0897      | 0.027*                           |
| C5  | -0.18463 (9)  | 0.24492 (12)  | 0.14072 (5) | 0.0202 (2)                       |
| H5  | -0.2489       | 0.1848        | 0.1503      | 0.024*                           |
| C6  | -0.07795 (9)  | 0.20660 (11)  | 0.16355 (4) | 0.0184 (2)                       |
| C7  | -0.06746 (9)  | 0.06157 (12)  | 0.19875 (5) | 0.0203 (2)                       |
| H7A | -0.0772       | 0.0857        | 0.2408      | 0.024*                           |
| H7B | -0.1307       | -0.0061       | 0.1874      | 0.024*                           |

|      |              |               |             |            |
|------|--------------|---------------|-------------|------------|
| C8   | 0.07275 (9)  | -0.04025 (11) | 0.13126 (5) | 0.0180 (2) |
| C9   | 0.02315 (9)  | -0.16067 (12) | 0.10144 (5) | 0.0218 (2) |
| H9   | -0.0295      | -0.2238       | 0.1214      | 0.026*     |
| C10  | 0.04935 (10) | -0.18974 (13) | 0.04328 (5) | 0.0252 (2) |
| H10  | 0.0139       | -0.2711       | 0.0235      | 0.030*     |
| C11  | 0.12743 (10) | -0.09959 (13) | 0.01412 (5) | 0.0261 (3) |
| H11  | 0.1471       | -0.1200       | -0.0255     | 0.031*     |
| C12  | 0.17656 (10) | 0.02068 (13)  | 0.04333 (5) | 0.0234 (2) |
| H12  | 0.2298       | 0.0824        | 0.0232      | 0.028*     |
| C13  | 0.14986 (9)  | 0.05357 (11)  | 0.10154 (5) | 0.0187 (2) |
| C14  | 0.20158 (9)  | 0.19445 (12)  | 0.12853 (5) | 0.0207 (2) |
| H14A | 0.2742       | 0.1667        | 0.1479      | 0.025*     |
| H14B | 0.2200       | 0.2657        | 0.0966      | 0.025*     |
| C15  | 0.13809 (10) | 0.20766 (12)  | 0.23032 (5) | 0.0225 (2) |
| H15A | 0.0759       | 0.2483        | 0.2550      | 0.027*     |
| H15B | 0.2116       | 0.2388        | 0.2479      | 0.027*     |
| C16  | 0.13116 (9)  | 0.03597 (12)  | 0.23015 (5) | 0.0221 (2) |
| H16A | 0.2053       | -0.0057       | 0.2172      | 0.027*     |
| H16B | 0.1166       | 0.0001        | 0.2705      | 0.027*     |

*Atomic displacement parameters (Å<sup>2</sup>)*

|     | $U^{11}$   | $U^{22}$   | $U^{33}$   | $U^{12}$    | $U^{13}$    | $U^{23}$    |
|-----|------------|------------|------------|-------------|-------------|-------------|
| N1  | 0.0199 (4) | 0.0179 (4) | 0.0205 (4) | -0.0011 (3) | -0.0002 (3) | -0.0007 (3) |
| N2  | 0.0207 (4) | 0.0183 (4) | 0.0192 (4) | -0.0001 (3) | 0.0008 (3)  | 0.0009 (3)  |
| C1  | 0.0212 (5) | 0.0159 (5) | 0.0190 (5) | 0.0006 (4)  | 0.0008 (4)  | -0.0029 (4) |
| C2  | 0.0248 (5) | 0.0167 (5) | 0.0251 (5) | -0.0013 (4) | 0.0030 (4)  | 0.0003 (4)  |
| C3  | 0.0309 (6) | 0.0186 (5) | 0.0238 (5) | 0.0033 (4)  | 0.0003 (4)  | 0.0022 (4)  |
| C4  | 0.0224 (5) | 0.0240 (5) | 0.0222 (5) | 0.0048 (4)  | -0.0012 (4) | -0.0032 (4) |
| C5  | 0.0203 (5) | 0.0207 (5) | 0.0196 (5) | -0.0001 (4) | 0.0030 (4)  | -0.0041 (4) |
| C6  | 0.0216 (5) | 0.0162 (5) | 0.0175 (5) | 0.0010 (4)  | 0.0030 (4)  | -0.0032 (4) |
| C7  | 0.0208 (5) | 0.0196 (5) | 0.0207 (5) | -0.0008 (4) | 0.0034 (4)  | 0.0014 (4)  |
| C8  | 0.0176 (5) | 0.0159 (5) | 0.0206 (5) | 0.0032 (4)  | -0.0004 (4) | 0.0016 (4)  |
| C9  | 0.0198 (5) | 0.0170 (5) | 0.0284 (6) | 0.0011 (4)  | -0.0015 (4) | 0.0005 (4)  |
| C10 | 0.0282 (6) | 0.0202 (5) | 0.0270 (6) | 0.0033 (4)  | -0.0059 (4) | -0.0045 (4) |
| C11 | 0.0323 (6) | 0.0260 (6) | 0.0199 (5) | 0.0074 (5)  | 0.0003 (4)  | -0.0020 (4) |
| C12 | 0.0243 (5) | 0.0227 (5) | 0.0231 (5) | 0.0034 (4)  | 0.0036 (4)  | 0.0029 (4)  |
| C13 | 0.0173 (5) | 0.0171 (5) | 0.0216 (5) | 0.0029 (4)  | -0.0001 (4) | 0.0013 (4)  |
| C14 | 0.0180 (5) | 0.0197 (5) | 0.0244 (5) | -0.0014 (4) | 0.0024 (4)  | 0.0006 (4)  |
| C15 | 0.0253 (5) | 0.0219 (5) | 0.0204 (5) | -0.0018 (4) | -0.0028 (4) | -0.0012 (4) |
| C16 | 0.0245 (5) | 0.0217 (5) | 0.0202 (5) | -0.0002 (4) | -0.0026 (4) | 0.0022 (4)  |

*Geometric parameters (Å, °)*

|        |             |        |             |
|--------|-------------|--------|-------------|
| N1—C1  | 1.4305 (14) | C8—C9  | 1.3970 (15) |
| N1—C15 | 1.4639 (14) | C8—C13 | 1.4053 (15) |
| N1—C14 | 1.4679 (13) | C9—C10 | 1.3873 (16) |
| N2—C8  | 1.4358 (14) | C9—H9  | 0.9500      |

|            |             |               |             |
|------------|-------------|---------------|-------------|
| N2—C16     | 1.4654 (14) | C10—C11       | 1.3874 (17) |
| N2—C7      | 1.4680 (14) | C10—H10       | 0.9500      |
| C1—C2      | 1.3991 (15) | C11—C12       | 1.3870 (17) |
| C1—C6      | 1.4051 (15) | C11—H11       | 0.9500      |
| C2—C3      | 1.3873 (16) | C12—C13       | 1.3964 (15) |
| C2—H2      | 0.9500      | C12—H12       | 0.9500      |
| C3—C4      | 1.3906 (16) | C13—C14       | 1.5236 (15) |
| C3—H3      | 0.9500      | C14—H14A      | 0.9900      |
| C4—C5      | 1.3877 (16) | C14—H14B      | 0.9900      |
| C4—H4      | 0.9500      | C15—C16       | 1.5315 (15) |
| C5—C6      | 1.3966 (15) | C15—H15A      | 0.9900      |
| C5—H5      | 0.9500      | C15—H15B      | 0.9900      |
| C6—C7      | 1.5262 (15) | C16—H16A      | 0.9900      |
| C7—H7A     | 0.9900      | C16—H16B      | 0.9900      |
| C7—H7B     | 0.9900      |               |             |
|            |             |               |             |
| C1—N1—C15  | 116.32 (9)  | C10—C9—C8     | 121.17 (10) |
| C1—N1—C14  | 112.87 (8)  | C10—C9—H9     | 119.4       |
| C15—N1—C14 | 112.85 (9)  | C8—C9—H9      | 119.4       |
| C8—N2—C16  | 115.58 (8)  | C9—C10—C11    | 119.81 (10) |
| C8—N2—C7   | 113.47 (8)  | C9—C10—H10    | 120.1       |
| C16—N2—C7  | 112.97 (8)  | C11—C10—H10   | 120.1       |
| C2—C1—C6   | 119.35 (10) | C12—C11—C10   | 119.34 (11) |
| C2—C1—N1   | 116.96 (9)  | C12—C11—H11   | 120.3       |
| C6—C1—N1   | 123.66 (9)  | C10—C11—H11   | 120.3       |
| C3—C2—C1   | 121.13 (10) | C11—C12—C13   | 121.78 (10) |
| C3—C2—H2   | 119.4       | C11—C12—H12   | 119.1       |
| C1—C2—H2   | 119.4       | C13—C12—H12   | 119.1       |
| C2—C3—C4   | 119.78 (10) | C12—C13—C8    | 118.60 (10) |
| C2—C3—H3   | 120.1       | C12—C13—C14   | 117.94 (9)  |
| C4—C3—H3   | 120.1       | C8—C13—C14    | 123.39 (9)  |
| C5—C4—C3   | 119.28 (10) | N1—C14—C13    | 115.16 (8)  |
| C5—C4—H4   | 120.4       | N1—C14—H14A   | 108.5       |
| C3—C4—H4   | 120.4       | C13—C14—H14A  | 108.5       |
| C4—C5—C6   | 121.86 (10) | N1—C14—H14B   | 108.5       |
| C4—C5—H5   | 119.1       | C13—C14—H14B  | 108.5       |
| C6—C5—H5   | 119.1       | H14A—C14—H14B | 107.5       |
| C5—C6—C1   | 118.54 (10) | N1—C15—C16    | 112.49 (9)  |
| C5—C6—C7   | 118.38 (9)  | N1—C15—H15A   | 109.1       |
| C1—C6—C7   | 122.97 (9)  | C16—C15—H15A  | 109.1       |
| N2—C7—C6   | 115.16 (8)  | N1—C15—H15B   | 109.1       |
| N2—C7—H7A  | 108.5       | C16—C15—H15B  | 109.1       |
| C6—C7—H7A  | 108.5       | H15A—C15—H15B | 107.8       |
| N2—C7—H7B  | 108.5       | N2—C16—C15    | 112.08 (9)  |
| C6—C7—H7B  | 108.5       | N2—C16—H16A   | 109.2       |
| H7A—C7—H7B | 107.5       | C15—C16—H16A  | 109.2       |
| C9—C8—C13  | 119.27 (10) | N2—C16—H16B   | 109.2       |
| C9—C8—N2   | 117.18 (9)  | C15—C16—H16B  | 109.2       |

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|               |             |                 |              |
|---------------|-------------|-----------------|--------------|
| C13—C8—N2     | 123.56 (9)  | H16A—C16—H16B   | 107.9        |
| C15—N1—C1—C2  | 147.34 (10) | C7—N2—C8—C13    | 97.36 (11)   |
| C14—N1—C1—C2  | -79.92 (11) | C13—C8—C9—C10   | 0.49 (16)    |
| C15—N1—C1—C6  | -34.51 (14) | N2—C8—C9—C10    | -179.77 (10) |
| C14—N1—C1—C6  | 98.24 (12)  | C8—C9—C10—C11   | 1.00 (16)    |
| C6—C1—C2—C3   | 1.33 (16)   | C9—C10—C11—C12  | -1.34 (17)   |
| N1—C1—C2—C3   | 179.57 (10) | C10—C11—C12—C13 | 0.20 (17)    |
| C1—C2—C3—C4   | 0.89 (17)   | C11—C12—C13—C8  | 1.28 (16)    |
| C2—C3—C4—C5   | -1.89 (16)  | C11—C12—C13—C14 | -175.68 (10) |
| C3—C4—C5—C6   | 0.67 (16)   | C9—C8—C13—C12   | -1.61 (15)   |
| C4—C5—C6—C1   | 1.54 (15)   | N2—C8—C13—C12   | 178.68 (9)   |
| C4—C5—C6—C7   | -174.80 (9) | C9—C8—C13—C14   | 175.18 (9)   |
| C2—C1—C6—C5   | -2.51 (15)  | N2—C8—C13—C14   | -4.53 (16)   |
| N1—C1—C6—C5   | 179.38 (9)  | C1—N1—C14—C13   | -50.30 (12)  |
| C2—C1—C6—C7   | 173.65 (10) | C15—N1—C14—C13  | 84.12 (11)   |
| N1—C1—C6—C7   | -4.46 (16)  | C12—C13—C14—N1  | 146.11 (10)  |
| C8—N2—C7—C6   | -49.21 (12) | C8—C13—C14—N1   | -30.70 (14)  |
| C16—N2—C7—C6  | 84.85 (11)  | C1—N1—C15—C16   | 86.36 (11)   |
| C5—C6—C7—N2   | 144.50 (10) | C14—N1—C15—C16  | -46.39 (12)  |
| C1—C6—C7—N2   | -31.66 (14) | C8—N2—C16—C15   | 86.95 (11)   |
| C16—N2—C8—C9  | 144.83 (9)  | C7—N2—C16—C15   | -46.09 (12)  |
| C7—N2—C8—C9   | -82.36 (11) | N1—C15—C16—N2   | -43.67 (13)  |
| C16—N2—C8—C13 | -35.45 (14) |                 |              |

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